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# A data-driven hybrid interval reactive power optimization based on the security limits method and improved particle swarm optimization

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The integration of renewable power generation introduces randomness and uncertainties in power systems, and the reactive power optimization with interval uncertainty (RPOIU) problem has been constructed to acquire the voltage control strategy. However, the large amount of uncertain data and the coexistence of discrete and continuous control variables increase the difficulty of solving the RPOIU problem. This paper proposes a data-driven hybrid interval reactive power optimization based on the security limits method (SLM) and the improved particle swarm optimization (IPSO) to solve the RPOIU problem. In this method, the large amount of historical uncertain data is processed by data-driven to obtain the boundary of optimal uncertainty set. The control variable optimization is decomposed into continuous variable optimization and discrete variable optimization. The continuous variables are optimized by applying the SLM with the discrete variables fixed, and the discrete variables are optimized by the IPSO with the continuous variables fixed. The two processes are applied alternately, and the values of the control variables obtained by each method are used as the fixed variables of the other method. Based on simulations carried out for the IEEE 30-bus system with three optimization methods, we verified that the voltage control strategy obtained by the data-driven hybrid optimization could ensure that the state variable intervals satisfied the constraints. Meanwhile, the values of the real power losses obtained by the proposed method were smaller than those obtained by the SLM and IPSO. The simulation results demonstrated the effectiveness and value of the proposed method.

#### KEYWORDS

renewable power generation, data-driven hybrid optimization, interval reactive power optimization, security limits method, particle swarm optimization

# **1** Introduction

Reactive power optimization is directly related to the security and economy of a power system. There is inherent randomness and volatility with renewable energy resources (RESs), including wind and photovoltaic power, so that the data of the RES output and the power load demand are generally uncertain in the power system. There will be voltage security problems under the effects of these uncertainties. Therefore, it is necessary to construct an uncertain reactive power optimization (URPO) strategy to realize voltage security control while handling the uncertainties. The URPO model incorporates the general reactive power flow (RPF) model with uncertain data, aiming at improving the voltage profile and reducing the loss.

Some approaches have been proposed to solve the URPO model, which is non-convex and non-linear. These approaches mainly include probabilistic programming, robust programming, and interval programming. The probabilistic approach acquires the specific probability distribution of the uncertain data, because it considers them to be random variables. This process represents the RPO model as an expectation model or chance-constrained programming model and obtains the results under a stated confidence level (Arefifar and Mohamed, 2014; Liu et al., 2016). Probabilistic programming requires a large amount of historical data, while the amount of data is generally limited, causing a bias of the empirical distribution. A data-driven modeling approach is introduced to address the issue, and the model is formulated as a two-stage problem, where the first-stage variables find the optimal control for discrete reactive power compensation equipment and the second-stage variables are adjusted to an uncertain probability distribution (Ding et al., 2018). A scenario-based two-stage stochastic optimization framework is also developed in (Saraswat et al., 2020) to minimize the total real power losses in the transmission network. To solve the URPO issue of two conflicting objective functions, the active power loss and voltage deviation are minimized simultaneously, and appropriate probability distribution functions are considered to model the stochastic behavior of wind and solar power generation with the Monte Carlo simulation (MCS) technique (Keerio et al., 2020). These probabilistic processes are quite time-consuming, and the probability distribution of uncertainties is rough due to the limited data.

In contrast, robust programming considers the uncertainties to be from various sets, such as box, cone, or ellipsoid sets, without assuming the probability distribution functions. A twostage distributed robust optimization model for optimal operation is formulated considering wind-power-uncertaintybased data-driven methods, where the polyhedra-based linearization method is introduced to approximate the secondorder cone power flow constraints with a series of linear constraints (Gao et al., 2021). To improve the computational performance, a second-order cone relaxation and decomposition algorithm is proposed to solve the multi-period reactive power optimization problem (Liu et al., 2017). The processes obtain the results with good robustness, while the accuracy of the robust programming model is low due to the linearization. Furthermore, there will be infeasible solutions sometimes because robust optimization is only applicable to convex models, while the general URPO model is non-convex.

The development of interval programming has addressed the issues of probabilistic and robust approaches. This approach expresses the uncertain data as intervals and therefore establishes the RPOIU problem in which the state variables are regarded as intervals. Notably, the control variables include both continuous (generator voltage) and discrete (transformer ratio and reactive power compensation) variables. Interval programming can ensure that the ranges of the state variables are completely confined within the security constraints. The methods for solving the RPOIU problem mainly include intelligent algorithms and mathematical processing. To solve the RPOIU model, the genetic algorithm (GA) is employed as the solution algorithm, where the reliable power flow calculation is used to judge the constraints of the model (Zhang et al., 2017). The improved genetic algorithm (IGA) is proposed to solve the problem that the simple GA is inefficient in the application of power system reactive power optimization, where the coding method, fitness function, initial population generation, and crossover and mutation strategy are modified (Chang and Zhang, 2017; Liu et al., 2022). Particle swarm optimization (PSO) is also widely applied to solve this problem (Li et al., 2017; Khan et al., 2020; Shri et al., 2021). An improved particle swarm optimization and Pareto archive algorithm are combined to solve the multi-objective reactive power optimization problem, and it outperforms the non-dominated sorting genetic algorithm II (NSGA-II) (Liu et al., 2021).

For the application of mathematical processing, the linear approximation method is formulated using the interval Taylor extension to help solve the RPOIU model (Jiang et al., 2014; Zhang et al., 2018b). In order to improve the accuracy of the approximation, the interval sequential quadratic programming method (ISQPM), which employs a second-order interval Taylor expansion, is proposed (Zhang et al., 2019). In addition, the security limits method (SLM) is defined to solve the RPOIU problem, and the model is switched to two deterministic reactive power optimization models (Zhang et al., 2018a).

It is noted again that the coexistence of discrete and continuous variables increases the difficulty of solving the RPOIU problem, and the accuracy when solving the problem by applying a single algorithm is generally low. Considering the above interval approaches, mathematical processing can deal with the continuous variables well, and intelligent algorithms are better at handling discrete variables. Therefore, the problem of mixed-variable processing can be addressed by a co-evolution method, which adopts a mathematical method to deal with continuous variables and an intelligent algorithm to deal with discrete variables to solve the RPOIU problem. The present work establishes a hybrid interval reactive power optimization algorithm considering the uncertainty of RESs. The algorithm uses interval programming to deal with uncertainties and decomposes the control variable optimization into two subproblems: continuous variable optimization and discrete variable optimization. Since the SLM can reduce the conservation of the interval reactive power optimization algorithm and has a better performance in searching for the optimal solution than other mathematical methods, the SLM is applied for continuous variable optimization. Since the PSO has faster convergence rate and simpler processes, the improved PSO (IPSO) is applied for discrete variable optimization. There are the algorithm alternations between these processes.

The construction of the RPOIU problem is presented in Section 2, followed by the hybrid optimization of the SLM and IPSO for solving the RPOIU problem in Section 3. The simulations employed to demonstrate the performance of the proposed method are presented in Section 4. The conclusions and contributions of this paper are given in Section 5.

## 2 Modeling of reactive power optimization with interval uncertainty (RPOIU) based on data-driven

As mentioned above, the large amount of historical uncertain data is processed by data-driven to obtain the boundary value of the uncertainties, and the input data of the power grid associated with uncertainties can be described as intervals, including power generation  $\hat{P}_{Gi}$ , active load demand  $\hat{P}_{Li}$ , and reactive load demand  $\hat{Q}_{Li}$ , which are expressed as  $[P_{Gi}^{\min}, P_{Gi}^{\max}]$ ,  $[P_{Li}^{\min}, P_{Li}^{\max}]$ , and  $[Q_{Li}^{\min}, Q_{Li}^{\max}]$ , respectively. The RPOIU problem is modeled with the real power losses  $P_{\text{loss}}$  as the objective function and power flow equations, security, and operational limits as constraints:

$$\min P_{\text{loss}} = \sum_{i \in \mathbb{S}} \sum_{j \in \mathbb{S}} V_i V_j G_{ij} \cos \theta_{ij}$$
(1)

s.t.

$$\begin{cases} \hat{P}_{Gi} - P_{Li} - P_i = 0, & i \in S'_G \\ Q_{Gi} - Q_{Li} - Q_i = 0, & i \in S'_G \end{cases}$$
(2)

$$\begin{cases} -\hat{P}_{Li} - P_i = 0, & i \in S_L \\ Q_{Ci} - \hat{Q}_{Li} - Q_i = 0, & i \in S_L \end{cases}$$
(3)

$$\begin{cases} P_{Gi} - P_{Li} - P_i = 0, & i \in S_{Gs} \\ Q_{Gi} - Q_{Li} - Q_i = 0, & i \in S_{Gs} \end{cases}$$
(4)

$$Q_{Gi}^{\min} \le Q_{Gi} \le Q_{Gi}^{\max}, \quad i \in S_G$$
(5)

$$Q_{Ci}^{\min} \le Q_{Ci} \le Q_{Ci}^{\max}, \quad i \in S_C$$
(6)

$$V_i^{\min} \le V_i \le V_i^{\max}, \quad i \in S_G \cup S_L \tag{7}$$

$$P_{Gi}^{\min} \le P_{Gi} \le P_{Gi}^{\max}, \quad i \in S_{Gs}$$

$$\tag{8}$$

$$T_l^{\min} \le T_l \le T_l^{\max}, \quad l \in S_{\mathrm{T}}$$
(9)

Here

$$P_{i} = V_{i} \sum_{j \in S} V_{j} \Big( G_{ij} \cos \theta_{ij} + B_{ij} \sin \theta_{ij} \Big)$$
(10)

$$Q_i = V_i \sum_{j \in S} V_j \Big( G_{ij} \sin \theta_{ij} - B_{ij} \cos \theta_{ij} \Big)$$
(11)

Moreover, S is the subset of whole system buses,  $S_G$  is the set of all generator buses,  $S'_{G}$  is the set of renewable power generator buses (except the slack bus), S<sub>Gs</sub> is the slack bus, where there is generally only one, SL is the set of load buses, SC is the index set of load buses with compensators, and ST is the index set of transformer branches. Eq. 1 is the objective function, where  $V_i$  and  $\theta_i$  are the voltage magnitude and bus angle at bus *i*, respectively,  $\theta_{ij} = \theta_i - \theta_j$ , and  $G_{ij}$  and  $B_{ij}$  are the real and imaginary parts of the admittance matrix, respectively. Eqs 2-4 are the power flow equations with interval uncertainties, where  $P_{Li}$  is the active load generation,  $P_{Gi}$  is the active power generation of slack bus,  $Q_{Gi}$  is the reactive power generation,  $Q_{Li}$ is the reactive load generation, Q<sub>Ci</sub> is the reactive power compensation of the capacitor,  $P_i$  (Eq 10) and  $Q_i$  (Eq 11) are the injected active and reactive power at bus *i*, respectively. Eqs 5–9 are the security and operational constraints, where  $T_l$  is the tap position of the transformer. The lower and upper limits of the variables are identified with the superscripts "min" and "max," respectively.

All the variables in the RPOIU model can be divided into state variables and control variables. The state variables include the voltage magnitudes of the load buses, bus angle, and reactive power generation. The control variables include the generator voltage, transformer ratio, and reactive power compensation. Therefore, the formulation of the RPOIU model can be simplified by expressing the vector of state variables as X and the set of control variables as  $\mu$ :

$$\min f (X, u) = [f^{L}, f^{U}]$$
  
s.t. 
$$\begin{cases} h(X, u) = [h^{L}, h^{U}] \\ g^{\min} \le g(X, u) \le g^{\max} \end{cases}$$
 (12)

where f(X, u) represents the real power losses of the RES power system, which is an interval and can be expressed as  $[f^{L}, f^{U}]$ ,  $[h^{L}, h^{U}]$  is the variation vector of the power input data in Eqs 2-4, and  $h^{L} = h^{U}$  represent the deterministic input data. g(X, u)represents all security and operational constraints,  $g^{\min}$  and  $g^{\max}$  are the lower and upper limits, respectively.

To express the model more conveniently, the bus order of the system is adjusted. Assuming that the slack bus is denoted by index 1, the number of all system buses is n, the number of generator buses is m (including the slack bus), the number of buses with the reactive power capacitor is r, and the number of transformers is k. The generator buses are denoted by index numbers in the range from two to m, the load buses are denoted by index numbers from m+1 to n, and the load buses with the reactive power capacitor are denoted by index numbers from m+1 to n.

m+1 to m + r. Therefore, the vectors of state and control variables are expressed as  $\mathbf{X} = [P_{G1}Q_{G1}\cdots Q_{Gm}V_{m+1}\cdots V_n\theta_2\cdots\theta_n]^T$  and  $\mathbf{u} = [V_2\cdots V_mQ_{Cm+1}\cdots Q_{Cm+r}T_1\cdots T_k]^T$ , respectively.

It is noted that the output of the reactive power compensator  $Q_{Cm+1} \cdots Q_{Cm+r}$  and transformer ratios  $T_1 \cdots T_k$  are discrete, and the voltages of the generators  $V_2 \cdots V_m$  are continuous for the control variable vector  $\boldsymbol{u}$ . There are interval variables within the state variable vector  $\boldsymbol{X}$ . Accordingly, the RPOIU problem is a non-linear model that requires the hybrid processing of continuous and discrete variables.

## 3 Hybrid optimization for solving the RPOIU problem based on security limits method (SLM) and improved particle swarm optimization (IPSO)

The hybrid interval reactive power optimization algorithm adopts the SLM and IPSO to process the RPOIU problem alternately. The SLM is applied to deal with the continuous variables in the model to improve the efficiency and optimization effect of the model and ensure that the load voltage is not off-limit in all scenarios. The IPSO is applied to deal with the discrete variables in the model to avoid the problem that the continuous rounding of discrete quantities may lead to inaccurate or even infeasible solutions. It is noted that the power flow equations with interval uncertainties are solved by the optimizing-scenarios method (OSM) (Zhang et al., 2018c).

# 3.1 SLM-based continuous variable processing

The RPOIU model is solved by the SLM under the condition that the discrete variables  $Q_{Ci}$  and  $T_l$  are fixed at stable values to obtain the optimal continuous variables  $V_i$  ( $i \in S'_G$ ). The specific process of the SLM is to define the determined security limits, and the interior point method (IPM) is used to solve the deterministic RPO model, which is modified by the security limits. Then, the optimal continuous variable is acquired.

Since the inequality constraints (5)–(9) in the RPOIU model are all univariate, the model can be expressed as follows:

min 
$$f(\mathbf{X}, \mathbf{u}) = [f^{L}, f^{U}]$$
  
s.t. 
$$\begin{cases} \mathbf{h}(\mathbf{X}, \mathbf{u}) = [\mathbf{h}^{L}, \mathbf{h}^{U}] \\ \mathbf{X}_{(1)}^{\min} \leq \mathbf{X}_{(1)} \leq \mathbf{X}_{(1)}^{\max} \\ \mathbf{u}^{\min} \leq \mathbf{u} \leq \mathbf{u}^{\max} \end{cases}$$
(13)

where  $X_{(1)}$  is a vector composed of the load bus voltage magnitudes and reactive power generation of the generator buses, and  $X_{(1)}^{max}$  and  $X_{(1)}^{min}$  are the upper and lower bounds,

respectively. The vector composed of bus angles and real power generation of the slack bus is denoted as  $X_{(2)}$ . Then, the vector of state variables is  $X = [X_{(1)}^T, X_{(2)}^T]^T$ .  $u^{\text{max}}$  and  $u^{\text{min}}$  are the upper and lower bounds of the vector of control variables u, respectively.

To obtain the maximum radii of the interval variables, a vector consisting of the maximum radii of the state variables is defined as  $\overline{\Delta X_{(1)}}$ , which is formulated as follows and can be computed through the OSM and MCS (Zhang et al., 2018a):

$$\overline{\Delta \boldsymbol{X}_{(1),i}} = \max_{\boldsymbol{u} = \boldsymbol{u} \leq \boldsymbol{u} \leq \boldsymbol{u} \leq \boldsymbol{u}} \left\{ \Delta \boldsymbol{X}_{(1),i} \mid \boldsymbol{h}(\boldsymbol{X}, \boldsymbol{u}) = \left[ \boldsymbol{h}^{L}, \boldsymbol{h}^{U} \right] \right\}$$
(14)

where  $\Delta X_{(1),i}$  is the radius of the *i*th variable in  $X_{(1)}$ .

According to  $\overline{\Delta X_{(1)}}$ , the security limits of the RPOIU model are defined as follows:

$$\begin{cases} AX_{(1)}^{\min} = X_{(1)}^{\min} + 2\overline{\Delta X_{(1)}} \\ AX_{(1)}^{\max} = X_{(1)}^{\max} - 2\overline{\Delta X_{(1)}} \end{cases}$$
(15)

Apparently, (15) represents the worst-case security bounds, while the difference between the security limit  $AX_{(1)}^{\min}$  (or  $X_{(1)}^{\max}$ ) and the original limit  $X_{(1)}^{\max}$  (or  $X_{(1)}^{\min}$ ) is close to  $\Delta X_{(1)}$ . In order to reduce the conservation of the proposed security limits, the interval ratio  $k^{I}$  is introduced to modify the definition of the security limits, and it is expressed as follows assuming that the control variables u are fixed at  $u_0 = (u^{\min} + u^{\max})/2$ :

$$\boldsymbol{k}^{I} = \frac{\boldsymbol{x}_{0} - \boldsymbol{X}_{0}}{\overline{\boldsymbol{X}_{0}} - \underline{\boldsymbol{X}_{0}}}$$
(16)

where  $\mathbf{x}_0$  represents the state variables acquired by solving the equations  $h(\mathbf{x}, \mathbf{u}_0) = (\mathbf{h}^L + \mathbf{h}^U)/2$ , and  $\underline{X}_0$  and  $\overline{X}_0$  are the lower and upper bounds of the state variable intervals obtained by solving the equations  $h(\mathbf{X}, \mathbf{u}_0) = [\mathbf{h}^L, \mathbf{h}^U]$ .

Assuming that the interval ratio corresponding to  $X_{(1)}$  is  $k_{(1)}^{l}$ , the security limits are modified as follows:

$$\begin{cases} SX_{(1)}^{\min} = X_{(1)}^{\min} + 2k_{(1)}^{I}\overline{\Delta X_{(1)}} \\ SX_{(1)}^{\max} = X_{(1)}^{\max} - 2(1 - k_{(1)}^{I})\overline{\Delta X_{(1)}} \end{cases}$$
(17)

where  $0 \le \mathbf{k}^I \le 1$ . It should be noted that there may be a violation when applying the modified security limits (17), because the interval ratio  $\mathbf{k}^I$  is defined at the midpoint of the control variables, while the state variables are not usually obtained at  $\mathbf{x}_0$ . Accordingly, the correction coefficients  $\delta_u$  and  $\delta_l$  are introduced to avoid the violation, and the corrected security limits are expressed as follows:

$$\begin{cases} S' \boldsymbol{X}_{(1)}^{\min} = S \boldsymbol{X}_{(1)}^{\min} + \delta_l \boldsymbol{X}_{(1)} \\ S' \boldsymbol{X}_{(1)}^{\max} = S \boldsymbol{X}_{(1)}^{\max} - \delta_u \boldsymbol{X}_{(1)} \end{cases}$$
(18)

where  $\delta_l X_{(1)}$  is the extent that  $X_{(1)}$  exceeds  $X_{(1)}^{\min}$ , and  $\delta_u X_{(1)}$  is the extent that  $X_{(1)}$  exceeds  $X_{(1)}^{\max}$ . If there is no violation,  $\delta_u X_{(1),i} = 0$  or  $\delta_l X_{(1),i} = 0$ .

Therefore, the RPOIU model can be transformed to a deterministic RPO model through Eqs 15–18, expressed as follows:

$$\min f(\mathbf{x}, \mathbf{u})$$

$$s.t. \begin{cases} h(\mathbf{x}, \mathbf{u}) = \boldsymbol{\xi} \\ S' \mathbf{X}_{(1)}^{\min} \le \mathbf{x}_{(1)} \le S' \mathbf{X}_{(1)}^{\max} \\ \mathbf{u}^{\min} \le \mathbf{u} \le \mathbf{u}^{\max} \end{cases}$$
(19)

where  $\boldsymbol{\xi}$  is any vector in the interval  $[\boldsymbol{h}^L, \boldsymbol{h}^U]$ , and  $f(\boldsymbol{x}, \boldsymbol{u})$  is the predictive value of the real power losses at the midpoint  $(\boldsymbol{h}^L + \boldsymbol{h}^U)/2$ . It is noted that if the state variables of deterministic model (16) are restricted within the security limits, the state variable intervals of the RPOIU model must be within their limits.

# 3.2 IPSO-based discrete variable processing

PSO is applied to deal with the discrete variables  $Q_{Ci}$  and  $T_l$  when solving the RPOIU model, and the continuous variables  $V_i$  ( $i \in S'_G$ ) are fixed. Each variable in the population is regarded as a particle in the PSO, and the position and speed of each particle can be obtained. It should be noted that the values of the state variables corresponding to the particles should satisfy the constraint condition. Accordingly, the fitness value corresponding to each particle can be acquired. The fitness value is the midpoint of the real power losses, and the corresponding fitness function has a penalty term.

The position of each particle in the search space is represented as  $X_i = (x_1, x_2, ..., x_n)$ , and the speed is represented as  $V_i = (v_1, v_2, ..., v_n)$ . The speed and position updating rules are expressed respectively as follows:

$$V_{i} = \omega \times V_{i} + c1 \times rand() \times (pBest_{i} - X_{i}) + c2 \times rand() \times (gBest - X_{i})$$
(20)

$$X_i = X_i + V_i \tag{21}$$

where *c*1 and *c*2 are the learning parameters, which are usually taken as 2, *rand* () is a random number within [0, 1], *pBest<sub>i</sub>* is the best solution of the *i*th particle, and *gBest* is the global best solution of the whole population.  $\omega$  is the inertia factor, which is formulated as follows by the linearly decreasing weight (LDW) strategy:

$$\omega(t) = (\omega_{ini} - \omega_{end})(Gk - t)/Gk + \omega_{end}$$
(22)

where  $\omega_{ini}$  is the initial inertia weight,  $\omega_{end}$  is the inertial weight at the maximum iteration number, Gk is the maximum number of iterations, and t is the current iteration time.

PSO is a global optimization method with a strong global search ability. However, it cannot make full use of the feedback information in the population, resulting in a poor local optimization ability, and the optimal value in the neighborhood of the  $pBest_i$  is often ignored. In order to address this issue, a local search around  $pBest_i$  is added in the PSO. The improvement of  $pBest_i$  is determined as follows:



$$pbest_{i} = \begin{cases} pbest_{i} + \omega \cdot step \cdot rand(), rand < 0.5\\ pbest_{i} - \omega \cdot step \cdot rand(), else \end{cases}$$
(23)

where *step* is the initial step length of the local search. The relationship between the global and local optima is well balanced through the improvement of  $pBest_i$ , allowing the algorithm to avoid falling into local optima and improving the accuracy of the PSO.

The discrete variables are processed by a crossover operation in the IPSO, including the crossover between the particle and itself and the crossover between the particle and optimal individuals. The crossover process can be expressed as follows:

$$u_i = \begin{cases} cu_i^{\max} \\ cu_i + (1-c)u_j \end{cases}$$
(24)

where  $u_i$  represents the discrete variables that require the crossover operation, *c* is a random number in [0,1],  $u_i^{\max}$  is the maximum of the transformer ratio and reactive power compensation, and  $u_j$  represents the optimal individuals including *pBest* and *gBest*.

# 3.3 Hybrid optimization based on SLM and IPSO

The RPOIU problem is solved through the hybrid optimization of SLM and IPSO. The values of the continuous variables obtained by SLM are applied as fixed continuous variable values in the IPSO, and the values of the discrete variables obtained by the IPSO are applied as fixed discrete variable values in the SLM. The two methods are applied to solve the RPOIU model alternately, and the values of the control variables are interactive. The final solution of the control variables when solving the RPOIU problem is obtained when the control variable values obtained by the two methods are consistent. Because the discrete variable values obtained by the IPSO are directly used by the SLM, the values of the continuous variables are used for the termination criterion. For convenience, in the example below, when the difference of the continuous variable values between the two methods was less than 0.01, the control variables values were considered to be approximately consistent. Accordingly, the detailed procedure of the hybrid optimization based on the SLM and IPSO is described as follows. It is noted again that the intervals of the state variables are obtained by using the OSM, and they should satisfy the constraints. The flow chart of the proposed method is presented in Figure 1.

The steps of the proposed algorithm are as follows:

Step (1) Input the power grid parameters and intervals of the power data and set the parameters of SLM and IPSO.

Step (2) Generate the initial values  $V_i^0$ ,  $Q_{Ci}^0$ , and  $T_l^0$  randomly in the feasible region of the control variables.

Step (3) Set  $V_i^{\text{fix}} = V_i^0$  and k = 1. Here,  $V_i^{\text{fix}}$  is the fixed value in the IPSO and k is the time of circulation.

Step (4) Keep  $V_i^{\text{fix}}$  stable and apply the IPSO to solve the RPOIU model to obtain the optimal discrete variables  $Q_{Ci}^k$  and  $T_l^k$ .

Step (5) Set  $Q_{Gi}^{\text{fix}} = Q_{Gi}^k$  and  $T_l^{\text{fix}} = T_l^k$ , where  $Q_{Gi}^{\text{fix}}$  and  $T_l^{\text{fix}}$  are the fixed values in the SLM, respectively.

Step (6) Keep  $Q_{Ci}^{\text{fix}}$  and  $T_l^{\text{fix}}$  stable and apply the SLM to solve the RPOIU model to obtain the optimal continuous variable  $V_i^k$ .

Step (7) Determine whether the difference between  $V_i^k$  and  $V_i^{k-1}$  is less than 0.01. If it is, stop the iteration process and print results. Otherwise, set  $V_i^{\text{fix}} = V_i^k$  and k = k + 1, then return to Step (4).

# 4 Simulation results

In this section, the simulations conducted for an IEEE 30-bus system are discussed to demonstrate the effectiveness and superiority of the hybrid optimization based on the SLM and IPSO in solving the RPOIU model problem. The results obtained by the proposed method are compared with those obtained by the SLM and IPSO. All parameters in the simulations were assigned values in a per-unit system, with 100 MV•A set as



the base power. All calculations were conducted using MATLAB with a 2.9-GHz CPU and 8 GB of RAM.

The IEEE-30 bus system included six generators (five renewable power generators), four transformers, and two capacitors. The topology of IEEE 30-bus system is shown in Figure 2. The active power generation and related variable ranges of the generators are shown in Table 1. The settings of the capacitors are shown in Table 2. The voltage magnitudes of the load buses were limited to the range of [0.95, 1.05]. The transformer ratios were limited to the range of [0.9, 1.1] with a step of 0.05. The parameters of SLM and IPSO are set as follows. The iteration precision  $\varepsilon = 10^{-4}$  in SLM. The number of iterations Size = 100, the population size M = 50, the learning factors c1 = c2 = 2, the initial inertia weight  $\omega_{ini} = 0.9$ , and the final inertia weight  $\omega_{end} = 0.1$  in IPSO.

According to the settings specified in Tables 1, 2, the proposed hybrid optimization strategy based on the SLM and IPSO was used to solve the RPOIU model problem for the IEEE 30-bus system, and the results were compared with those obtained by the SLM and IPSO. The results obtained by the hybrid optimization, SLM, and IPSO for the IEEE 30-bus system are presented inFigures 3, 4. Figure 3A; Figure 4A show the voltage magnitude intervals acquired by the hybrid optimization, SLM, and IPSO. The interval bounds were all within the voltage limits. The boundary of state variable intervals obtained by the SLM was closer to the security limits than the hybrid optimization and IPSO. The intervals obtained by the hybrid optimization were close to that obtained by IPSO. Figure 3B; Figure 4B present the reactive power generation intervals acquired by the hybrid optimization, SLM, and IPSO. The interval bounds also were within the limits of the reactive power generation and the interval results obtained by the three methods were close for most of the buses. The results

Bus number	Active power generation	Reactive power output		Voltage magnitude	
		Lower bounds	Upper bounds	Lower bounds	Upper bounds
1	-	-0.2	1.5	0.9	1.1
2	0.8	-0.2	0.6	0.9	1.1
5	0.5	-0.15	0.63	0.9	1.1
8	0.2	-0.15	0.5	0.9	1.1
11	0.2	-0.1	0.4	0.9	1.1
13	0.2	-0.15	0.45	0.9	1.1

### TABLE 1 Active power generation and related variable ranges of generators in IEEE 30-bus system (p.u.).

TABLE 2 Settings of capacitors in IEEE 30-bus system (p.u.).

Bus number	Lower bounds	Upper bounds	Variation step
10	0	0.5	0.1
24	0	0.1	0.02



verified the effectiveness of the proposed method for solving the RPOIU problems. The reasons for ensuring the interval results within voltage limits or reactive power generation limits were that the hybrid optimization and SLM both used the security limits to ensure the feasibility of the control variables, and the IPSO determined the feasibility of the control variables by judging whether the state variable intervals satisfied the constraints of the RPOIU model. Figure 5 presents the iterative convergence process of the three algorithms, and the

results are shown in Table 3. The hybrid optimization achieved the minimum real power loss, and the IPSO had a relatively large loss of active power compared to the other algorithms. This was because the hybrid optimization could obtain better solutions for the continuous and discrete variables, in contrast to the single optimization, which had difficulty dealing with mixed control variables. It demonstrated that the proposed method had higher accuracy than SLM and IPSO for solving RPOIU models.





TABLE 3 Values of real power losses optimized by the hybrid optimization, SLM, and IPSO.

	Hybrid Optimization	SLM	IPSO
Real power losses [p.u.]	0.0498	0.0507	0.0528

# **5** Conclusion

This paper proposed a data-driven hybrid interval reactive power optimization based on SLM and IPSO for

solving the RPOIU problem to address the issue of dealing with mixed control variables. The large amount of uncertain data is expressed as intervals based on data-driven, and the control variable optimization is decomposed into continuous variable optimization and discrete variable optimization. For reducing the conservation of the interval algorithm, the SLM is applied for continuous variable optimization and the IPSO is applied for discrete variable optimization. The two processes are used to solve the RPOIU problem alternately and iteratively until the control variables optimized by the two processes are consistent.

The simulation results obtained by the proposed datadriven hybrid interval reactive power optimization for the IEEE 30-bus system were compared with those obtained by the SLM and IPSO. The proposed data-driven hybrid interval reactive power optimization acquired smaller real power losses than the SLM and IPSO, and it ensured that the interval bounds of the state variables remained within the constraints. The simulation results verified the effectiveness and advantages of the proposed method.

## Data availability statement

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding author.

## Author contributions

DC conceptualized the study, contributed to the study methodology, and wrote the original draft. SQ

contributed to the writing—review and editing, data curation and investigation. QL contributed to study methodology, data analysis, wrote the original draft and writing-review. WX contributed to software and paper revision. XL contributed to investigation and writing—original draft. YL contributed to supervision and writing—review and editing. HY contributed to the revision of the paper. NK contributed to editing of the paper. All authors have read and agreed to the published version of the manuscript.

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# Conflict of interest

Authors DC, SQ, WX and XL were employed by the State Grid Hunan Electric Power Co., Ltd.

The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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